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	$c_{int} = \frac{m_{Az_2O_3} \cdot F_{Az_1Az_2O_3}}{C_{int}} + \frac{m_{Az_2O_3} \cdot F_{Az_1Az_2O_3}}{C_{int}}$	$\cdot P \cdot m$	$\mu \cdot \rho_{int} \cdot n$	l _{ss_dd}									
1	m ₃₃	$t \cdot m_{lot} \cdot K$	$\cdot m_{dl}$										
		estimated		probability		standard uncertainty		sensitivity	uncertainty				
2	parameter	value	specification	distribution	divisor	(u)	sensitivity coefficient (c.)	(c.)	(c,u)	abs			
							$m_{Az_1O_1} \cdot F_{Az_1Az_2O_1} \cdot m_{zz} \cdot \rho_{az} \cdot m_{zz_add}$						
					√3		m_{ii} , $m_{i\sigma} \cdot K \cdot m_{di}$						
- 3	Punty (P)	39,50%	0,10%	неспеск		0,00057735	E P P P C P	0,000112682	6,5057E+08	6,5057E+08	TIOT HERCK	centricate	
	mass of arsenic oxide in stock						* e (.e.) 01 * ma Pau ma_di						
4	solution in g (m _{ks200})	0,1853	1602MP 40+0,2			0,000167986	m _{iii_t} m _{int} K m _{di}	0,000605065	1,01642E-07	1,01642E-07	uncertainty of	fibalance 1	
	total mass of stock solution in o						$= \frac{m_{\mu_1\phi_1} \cdot F_{\mu_1\mu_1\phi_1} \cdot P \cdot m_{\mu} \cdot \rho_{\mu} \cdot m_{\mu_{\mu}\mu_{\mu}}}{m_{\mu_{\mu}\mu_{\mu}}}$						
5	(m _{111,2})	499,41	PL1200 200+50	0		0,065721047	$m_{m_{2l}}^* \cdot m_{2l} \cdot K \cdot m_{2l}$	-2,24502E-07	-1,47545E-00	1,47545E-00	uncertainty of	f balance 2	
							$m_{\mathcal{R}_{1}\mathcal{O}_{1}} \cdot P \cdot m_{ii} \cdot \rho_{iii} \cdot m_{ii} di$						
6	(Faulantic)	0.75739018				0	$m_{a-i} \cdot m_{ia} \cdot K \cdot m_{di}$	0.000148033			from UPAC o	lata: uncertain	ty negligible
							mea Fried P.m. P.						
	mass of stock solution in diluted		CL 1000 000 00	0			$m_{\mu} \rightarrow m_{\mu} + K \rightarrow m_{\pi}$		1 120226 02				
ŕ	Banation (met.al.)		101200 200120	NV		4,414164865	m E P.m. C.m	1,121105-99	1,128220-00	1,138236-00	uncertainty s	rualanue 2	
							$-\frac{m_{A_{1}}\sigma_{1} + a_{A_{1}}\sigma_{1} + a_{A_{1}}\sigma_{1} + a_{A_{1}}\sigma_{1}}{m_{A_{1}}\sigma_{A_{1}}\sigma_{A_{1}} + a_{A_{1}}\sigma_{A_{1}}\sigma_{A_{1}}}$						
8	mass of diuted solution (mp)	396,45	PL1200 200+10	00		0,039310953	m ₂ , m ₂ , m ₂	-1,12518E-07	-4,42319E-09	4,42319E-09	uncertainty of	f balance 2	
							$m_{Au_1o_1} \cdot F_{Au_1Au_1o_1} \cdot P \cdot m_u \cdot m_{uu_u}$						
9	density of the lot in g/l $(\mathfrak{g}_{\mathrm{cr}})$	997,907535				0,06596093	$m_{\mu_{i}} \cdot m_{i\mu} \cdot K \cdot m_{di}$	1,12354E-07	7,41095E-09	7,41095E-09	see separate	calculation	
	and a start of a start of a start of a start of a						$m_{,\omega_1,0_1} \cdot F_{,\omega_1,\omega_1,0_1} \cdot P \cdot \rho_{\omega_1} \cdot m_{\omega_1,d_1}$						
10	in g (mas)	200	PL1200 200-20	0		0,010160985	$m_{w_{w_{w_{w_{w_{w_{w_{w_{w_{w_{w_{w_{w_$	5,605936-07	5,69617E-09	5,69617E-09	uncertainty of	fibalance 2	
							$m_{\mu_{\ell}\sigma_{\ell}} \cdot F_{\mu_{\ell},\mu_{\ell}\sigma_{\ell}} \cdot P \cdot m_{\mu} \cdot \rho_{\mu\ell} \cdot m_{\mu_{\mu},\mu_{\ell}}$						
	tatal mass of the latin o (m.)	40070	BEWORD			34 00404405	$m_{u_{u_{u_{u_{u_{u_{u_{u_{u_{u_{u_{u_{u_$	2 246305.00	7.000048-00	7.000046.00	un cartalature	Charleson 2	
	the many of the latter y (rigg)						$m_{\mu,0} \cdot F_{\mu',\mu,0} \cdot P \cdot m_{\mu'} \cdot \rho_{\mu'} \cdot m_{\mu',\mu'}$				and a many a		
							$m_{\mu_{el}} \cdot m_{\mu} \cdot K^2 \cdot m_{\mu}$						
12	bouyancy correction factor (K)	1,00103149				0,00011		-0,000112003	-1,23203E-08	1,23203E-08	from PTB info	rmations	
				how									
13	resuit (gil)	0,00011212	_	total distance	many of the lot	(in o (mint)		He .	1,45046E-07				
				married stock a	okaioo in the los	in almost							
14	result in mg1	0,11211854											
					mang or owno	an ger (mort)							
15	standard uncertainty in mol	0.00014606		ma	IS OF BRUKED SOF								
1			masse	of stock polution is	a diluted polution	n (mss_dil)							
				quotient of moleo	ular masses (F)	As/As203)							
16	rei, uncertainty	0,13%		total mass of	took solution it	· g (mes_t)							
			mass of a	esenio oxide in sto	ck solution in g	(mAs203)							
17	exp. uncertainty	0,00029009				Purity (P)							
						0,E+00	2,E-08 4,E-08 6,E-08 8,E-08 1,E-07 1,E-07						
10	exp. rel. uncertainty	0,26%						1					
	Koch M	Measu	rement i	incertair	ntv revi	sited - 9	ADCMET PT Workshop 200	7 Dar es	Salaam			13 7	10
	10001, 11.	wicasu	i cinicint t	anoci tali	1.9 10 16		2001 2001 2001 2001	Dar Co	Julaaill			-	



































































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	 Method and Laboratory bias u(bias) – method 2 Use of PT results In order to have a reasonably clear picture of the bias from interlaboratory comparison results, a laboratory should participate at least 6 times within a reasonable time interval 								
	Uncertainty component from the uncertainty of the nominal value								
	between laboratory standard deviations ${\rm s}_{\rm R}$	${\rm s}_{\rm R}$ has been on average 9% in the 6 exercises							
1	Convert to relative uncertainty $u(C_{ref})$	Mean number of participants= 12 $u(C_{ref}) = \frac{s_R}{\sqrt{n}} = \frac{9\%}{\sqrt{12}} = 2.6\%$							
0	or: $u(C_{ref}) = 1.25 \cdot \frac{s_R}{\sqrt{n}}$ for a robust mean t with ISO 13528	o be in accordance							
	Koch, M.: Measurement uncertainty revisited – SADCMET PT Workshop 2007 Dar es Salaam								



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 Method and Laboratory bias u(bias) – method 3 From Recovery Tests Recovery tests, for example the recovery of a standard addition to a sample in the validation process, can be used to estimate the systematic error. In this way, validation data can provide a valuable input to the estimation of the uncertainty. 							
uncertainty component from spiking							
uncertainty of the concentration of the spike u(conc)	from the certificate: 95% confidence intervall = \pm 1.2 % u(conc) = 0.6 %						
uncertainty of the added volume u(vol)	from the manufacturer of the micro pipette: max. bias: 1% (rectangular interval), repeatability: max. 0.5% (standard dev.) $u(vol) = \sqrt{\left(\frac{1\%}{\sqrt{3}}\right)^2 + 0.5\%^2} = 0.76\%$						
uncertainty of the spike u(c _{recovery})	$\sqrt{u(conc)^2 + u(vol)^2} = \sqrt{0.6\%^2 + 0.76\%^2} = 1.0\%$						
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